

September 2019 UD18-057

Functional Servicing Report







Project: 2993-3011 Sheppard Avenue East & 1800-1814

Pharmacy Avenue

Sheppard Pharmacy GP Inc.

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Functional Servicing and Stormwater Management Report

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City of Toronto

Functional Servicing and Stormwater Management Report

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Functional Servicing and Stormwater Management Report

Executive Summary

Lithos Group Inc. (Lithos) was retained by Sheppard Pharmacy GP Inc. (the "Owner") to prepare a Functional Servicing and Stormwater Management Report in support of a Rezoning Application, for a proposed mixed-use development south-west of the intersection between Sheppard Avenue East and Pharmacy Avenue, at 2993-3011 Sheppard Avenue East & 1800-1814 Pharmacy Avenue (M1T 3J5), in the City of Toronto (the "City"). The following summarizes our conclusions:

Storm Drainage

More details for the Stormwater Management (SWM) Section of this report will be prepared during the Site Plan Application stage. The site stormwater discharge will be controlled to the 2-year predevelopment flow and will be connected to the existing 675 mm diameter storm sewer on Pharmacy Avenue. In order to achieve the target flows and meet the City's Wet Weather Flow Management Guidelines (WWFMG), quantity controls will be utilized and up to 198.7 m³ of storage will be required. The stormwater management (SWM) system will be designed to provide enhanced level (Level 1) protection as specified by the Ministry of the Environment, Conservation and Parks (MECP). During Site Plan Application, a detailed analysis will be provided to assess the water quality on site and determine additional measures in order to achieve a minimum total suspended solids (TSS) removal of 80%.

Sanitary Sewer

The flow from the proposed development will be directed to the existing 250 mm diameter sanitary sewer on Pharmacy Avenue. The additional net discharge flow from the proposed development, is anticipated at approximately 8.39 L/s. A Model Analysis is underway to determine the capacity of the existing sanitary sewer network along Pharmacy Avenue to accommodate the additional flow from the proposed development.

Water Supply

Water supply for the site will be from the existing 300 mm diameter watermain on the east side of Pharmacy Avenue. It is anticipated that a total design flow of 136.26 L/s will be required to support the proposed development. The results of the hydrant flow test reveal that the existing water infrastructure can support the proposed development.

Site Grading

The proposed grades will improve the existing drainage conditions to meet the City's/Regional requirements. Grades will be maintained along the property line wherever feasible and emergency overland flow will be directed to Sheppard Avenue East.

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1.0 Introduction

Lithos Group Inc. (Lithos) was retained by Sheppard Pharmacy GP Inc. (the "Owner") to prepare a Functional Servicing and Stormwater Management Report in support of a Zoning Application for a proposed mixed-use development located south-west of the intersection between Sheppard Avenue East and Pharmacy Avenue in the City of Toronto (City).

The purpose of this report is to provide site-specific information for the City's review with respect to infrastructure required to support the proposed development. More specifically, the report will present details on sanitary discharge, water supply and an outline of the storm drainage pattern.

We contacted the City's engineering department to obtain existing information in preparation of this report. The following documents were available for our review:

- Plan and profile drawings of:
 - o Pharmacy Avenue, drawing No. 61M-2, dated September 1960;
 - Pharmacy Avenue, drawing No. W-145, dated November 1956;
 - Sheppard Avenue East, drawing No. 71M-1, dated January 1963;
 - Sheppard Avenue East, drawing No. 1228-A, dated February 1966;
 - o Sheppard Avenue, drawing No. 1228-C, dated October 1967
- Toronto CUMAP Digital Sewer/Water Network of the area surrounding the site;
- Sewer / Water atlas maps;
- Site Plan prepared by Kirkor Architects + Planners, dated September 10, 2019;
- Statistics prepared by Kirkor Architects + Planners, dated September 10, 2019;
- Topographical Survey prepared by Schaeffer Dzaldov Bennett Ltd., dated April 2, 2018; and
- Hydrogeological Assessment prepared by Arcadis, dated May 28, 2019.

2.0 Site Description

The existing site is approximately 0.658 hectares and is comprised of two (2) single-storey commercial buildings with outdoor parking area. The site is located on the south-west corner of the intersection between Sheppard Avenue East and Pharmacy Avenue and is bound by residential development to the west and south, Sheppard Avenue East to the north and Pharmacy Avenue to the east. Refer to **Figures 1** and **2** following this report and site photographs in **Appendix A**.

The City's Basement Flooding Protection program is a multi-year program that is helping to reduce the risk of future flooding by making improvements to the City's sewer system and overland drainage routes. As part of this program, Environmental Assessment Studies are conducted in basement flooding study areas across the City. According to the BFPP EA STUDY STATUS Map, provided in **Appendix B**, the subject development is located in Study Area 30 into which, EA studies are completed. Further direction is anticipated from the City for additional measures to reduce flooding risk, if applicable.

3.0 Site Proposal

The proposed mixed-use development will include a 21-storey building and it will be serviced by three (3) levels of underground parking. It will consist of 433 residential units with a total Gross Floor Area (GFA) of 27,968.08 m² and retail area with a GFA of 1,340.00 m². The proposed development will include a total 29,308.00 m² of GFA. Please refer to **Appendix B** for the proposed site plan and site statistics.

4.0 Terms of Reference and Methodology

4.1. Terms of Reference

The Terms of Reference used for the scope of this report was based on the City's Development Guide Servicing Report Terms of Reference, December 2007, the November 2009 First Edition of the City of Toronto Design Criteria for Sewers and Watermains and the November 2006 Wet Weather Flow Management Guidelines (WWFMG).

4.2. Methodology: Stormwater Drainage and Management

This report provides a brief Stormwater Management (SWM) review of the pre-development and post-development conditions and comments on opportunities to reduce peak flows. A detailed Stormwater Management (SWM) report will be prepared at the Site Plan Application stage.

The proposed development will be designed to meet the City's WWFMG and the standards of the Province of Ontario as set out in the Ministry of Environment, Conversation and Parks (MECP) 2003 Stormwater Management Planning and Design Manual (SWMPD). The following design criteria will be reviewed:

- Post-development peak flow for the 100-year storm event from the site should be controlled to the 2-year target flow;
- A specified rainfall depth of 5 mm is to be retained on-site, as required by the WWFMG;
- A safe overland flow will be provided for all flows in excess of the 100-year storm event.

4.3. Methodology: Sanitary Discharge

The sanitary sewage discharge from the site will be determined using sanitary sewer design sheets that incorporate the land use and building statistics as supplied by the design team. The calculated values provide peak sanitary flow discharge that considers infiltration.

The estimated sanitary discharge flows from the proposed site will be calculated based on the criteria shown in **Table 4-1** below.

Table 4-1 - Sanitary Flows

Usage	Design Flow	Units	Population Equivalent
			1 Bedroom Unit = 1.4 ppu
Residential	240	Library / samiba / day	2 Bedroom Unit = 2.1 ppu
		Litres / capita / day	3 Bedroom Unit = 3.1 ppu
Commercial / Retail	250		1.1 p/100 m ²

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Based on the calculated peak flows, the adequacy of the existing infrastructure to support the proposed development will be discussed.

4.4. Methodology: Water Usage

The domestic water usage was calculated based on the City's design criteria outlined in Table 4-2 below.

Table 4-2 – Water Usage

Usage	Water Demand	Units
Residential	191	Litres / capita / day
Commercial / Retail	5	Litres / 1.0 m² / day

Pressure and flow testing has been conducted on the existing hydrants located near the site along Pharmacy Avenue to obtain existing flows, residual and static pressure.

5.0 Stormwater Management and Drainage

5.1. Existing Conditions

According to available records, there are two (2) existing storm sewers, a 675 mm concrete storm sewer on Pharmacy Avenue flowing south and a 450 mm concrete storm sewer on Sheppard Avenue West flowing west.

The existing site contains two (2) commercial developments with parking area. Stormwater from the property is collected by private catchbasins, eventually draining into the City's existing storm sewer network at Pharmacy Avenue.

The existing site is primarily covered by buildings and asphalt paved area, thus there no significant infiltration onsite. Although the existing run-off coefficient is estimated between 0.90, the WWFMG requires target flow calculations based on a run-off coefficient of 0.5. **Table 5-1** shows the input parameters which are illustrated on the pre-development drainage area plan in **Figure DAP-1** in **Appendix C**.

Table 5-1 – Target Input Parameters

Catchment	Drainage Area (ha)	С	Tc (min.)
A1 Pre	0.658	0.50	10

Peak flows calculated for the existing conditions are shown in **Table 5-2** below. Detailed calculations are in **Appendix C**.

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Table 5-2 – Target Peak Flows

	Peak Flow Rational Method			
Catchment	(L/s)			
	2-year	5-year	100-year	
A1 Pre	80.6	120.4	228.8	

As shown in **Table 5-2**, the post-development flows towards Sheppard Avenue East and Pharmacy Avenue, will need to be controlled to the target flow of 80.6 L/s.

5.2. Stormwater Management

In order to meet the WWFMG criteria, the development flow rate is to be controlled to the two (2)-year target flow established in **Section 5.1**. Overland flow from the site will be directed towards the adjacent right-of-ways.

The post-development drainage areas and runoff coefficients are indicated on **Figure DAP-2**, located in **Appendix C** and summarized in **Table 5-3** below.

Table 5-3 - Post-development Input Parameters

Drainage Area	Drainage Area (ha)	"C"	Tc (min.)
A1 Post	0.658	0.50	10

5.2.1. Water Balance

As required by the City's WWFMG, a rainfall depth of 5 mm must be retained over the entire parcel area. A 5 mm rainfall over the entire site equates to a required water balance volume of 32.92 m³. In order to achieve this, low impact development (LID) techniques may be implemented:

- collecting rainwater in storage tanks to be reused for irrigation purposes,
- Green Roof and Planters

Detailed calculations will be provided during the detailed design stage of Site Plan Application.

5.2.2. Quantity Controls

Using the City's intensity-duration-frequency (IDF) data, modified rational method calculations were undertaken to determine the maximum storage required during each storm event. Results for the 2, 5, and 100-year storm events are provided in **Table 5.4**. The detailed post-development quantity control calculations are provided in **Appendix C**.

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Storm Event	Storm Event	Target Flow (L/s)	Required Storage Tank Volume (m³)
	2-year		38.7
A1 Post	5-year	80.6	81.7
(Controlled)	100-year		198.7

Table 5.4 – Post-development Quantity Control as Per City Requirements

As shown in **Table 5.4**, in order to control post-development flows to 2-year pre-development conditions, a target flow of 80.6 L/s is to be satisfied. The required on site storage is calculated at 198.7 m³ for the 100-year storm event. This can be achieved through the design and installation of stormwater holding tanks, flow control devices and/or roof storage, details of which will be provided through the detailed design stage of Site Plan Application.

5.2.3. Quality Controls

Stormwater treatment must meet Enhanced Protection criteria as defined by the MECP 2003 SWMPD Manual, including the removal of at least 80% total suspended solids (TSS). Quality control and the need of additional measures is required, details of which will be discussed during Site Plan Application.

5.3. Proposed Storm Connection

The storm sewer system will be designed to meet the City's requirements and discharge into the existing 675 mm diameter storm on Pharmacy Avenue via a 200 mm diameter storm sewer service connection with a minimum grade of 2.00% (or equivalent design). Orifice controls, if required, will be designed to meet the allowable release rates to the municipal system and will be defined at the detailed design stage. The 'Proposed Servicing Plan' Figure-3 in Appendix F indicates the stormwater service connection.

6.0 Groundwater Conditions

According to the Hydrogeological Assessment prepared by Arcadis Canada Inc., May 28, 2019, water table ranges between 164.62 and 177.82 m asl. Furthermore, the proposed development will be serviced by three (3) underground parking levels and the slab of the P3 parking will be at an elevation between 167.55 and 167.45 m asl approximately 10m below the ground surface. Therefore, due to the fact that the proposed development will be partially submerged into the groundwater table, long-term and short-term groundwater discharge will be required.

The results of groundwater sampling on site, reveal that groundwater quality limits according to the City's by-laws are not met for discharging into the existing sanitary network (refer to **Appendix B**). Therefore, a treatment facility will be required prior to discharging into the City's infrastructure both for short-term and long-term dewatering of the site.

6.1. Short-Term Dewatering

According to the Hydrogeological Assessment prepared by Arcadis Canada Inc., May 28, 2019, short-term groundwater discharge during construction is estimated at 101,300 L/day which translates to 1.17 L/s.

6.2. Long-Term Dewatering

Given that the underground construction will be partially submerged into the existing groundwater table, long-term groundwater discharge, along with the installation of a permanent dewatering system, will be required. According to the Hydrogeological Assessment prepared by Arcadis Canada Inc., May 28, 2019, groundwater flow rate of 15,800 L/day is estimated to be discharged to the City's Sewer Infrastructure. As mentioned above, groundwater is not in compliance with the City of Toronto sanitary and combined sewer quality limits, therefore, after being collected by the building's sub-drain system, it will be treated and then pumped into the City's sanitary sewer network, along Pharmacy Avenue.

The capacity of the existing sanitary sewer network along Pharmacy Avenue to accommodate the total post-development flows, will be discussed under **Section 7.0** of this report.

7.0 Sanitary Drainage System

7.1. Existing Sanitary Drainage System

The existing site is comprised of two (2) single-storey commercial buildings with parking area. According to available records, there is a 250 mm diameter sanitary sewer along Pharmacy Avenue, flowing south and a 250 mm diameter sanitary sewer at the north side of Sheppard Avenue East, flowing west. The sewers on Pharmacy Avenue and Sheppard Avenue East connect to the 350 mm diameter sanitary trunk sewer on Farmcrest Drive.

7.2. Existing and Proposed Sanitary Flows

The sanitary flow generated by the proposed development at 2993-3011 Sheppard Avenue East & 1800-1814 Pharmacy Avenue was compared to the existing flow in order to quantify the net increase in the sanitary sewer.

Using the design criteria outlined in **Section 4.3** and existing site information, the sanitary discharge flow from the existing commercial buildings is estimated at 0.25 L/s. Detailed calculations can be found in **Appendix D**.

Similarly, using the design criteria and the proposed development statistics, the new building will discharge 8.63 L/s (8.45 L/s sanitary flow and 0.18 L/s groundwater flow) into the City's infrastructure.

The additional flow will be considered within the sanitary discharge rate, therefore, there is an increase in sanitary flow of approximately 8.39 L/s within the City's sewer network.

Since the long-term flow (sanitary and long-term groundwater flow) into the City's Sanitary Infrastructure is more than the flow during construction (short-term groundwater flow), a Model Analysis is underway, to determine the capacity of the existing sanitary sewer network along Pharmacy Avenue to accommodate the flow from the proposed development.

7.3. Proposed Sanitary Connection

The proposed development will connect to the existing 250 mm diameter sanitary sewer on Pharmacy Avenue through a 200 mm diameter sanitary sewer connection at a minimum grade of 2.00% (or equivalent pipe design). Refer to 'Proposed Servicing Plan' Figure-3 in Appendix F, for the proposed sanitary connection.

8.0 Water Supply System

8.1. Existing System

The existing watermain system consists of a 300 mm and a 1050mm diameter watermains on the east and west side of Pharmacy Avenue respectively and a 300 mm and a 1350 mm diameter watermains on the north and south side of Sheppard Avenue East respectively. Hydrant flow tests were carried out by Urban X on June 7, 2019 along Pharmacy Avenue to determine the flow and pressure in the existing watermain network. The results of the test indicate the existing static pressure is 386.1 KPa (56 psi) and 73.37 L/sec (1163 USPGM) of water is available with a residual pressure of 330.9 KPa (48 psi). The full detailed report is included in **Appendix E**.

8.2. Proposed Water Supply Requirements

The estimated water consumption was calculated based on the occupancy rates shown on **Table 4-2**, based on the City's watermain design criteria revised in November 2009. It is anticipated that an average consumption of approximately 1.77 L/s (153,006 L/day), a maximum daily consumption of 2.92 L/s (252,460 L/day) and a peak hourly demand of 4.39 L/s (15,811 L/hr) will be required to service this development with domestic water. Detailed calculations can be found in **Appendix E**.

The fire flow requirements were estimated using the method prescribed by the Fire Underwriters Survey (FUS) be undertaken to assess the minimum requirement for fire suppression. The fire flow calculations are normally conducted for the largest storey, by area, and for the two immediately adjacent storeys. **Table 8-1** illustrates the input parameters used for the FUS calculations. According to our calculations, a minimum fire suppression flow of approximately 133.33 L/s (2,113 USGPM) will be required. Refer to detailed calculations found in **Appendix E**.

	Frame used	Combustibility of Contents Presence of Sprinklers	Presence	Separation Distance			
Parameter	for Building			North	East	South	West
Value according to FUS options	Fire- Resistive Construction	Limited- Combustible	Yes	Road	Road	3.1m to 10.0m	3.1m to 10.0m
Surcharge/reduction from base flow	0.6	15%	30%	0%	0%	20%	20%

Table 8-1 - Fire Flow Input Parameters

In summary, the required design flow is the sum of 'the minimum fire suppression flow' and 'maximum daily demand' (133.33+2.92 = 136.26 L/s, 2,160 USGPM).

The results of the hydrant flow test carried out by Urban X on June 7, 2019 along Pharmacy Avenue, reveal that the existing water infrastructure has 2,620 USGPM (165.3 L/s) at 20psi and will support the proposed development. The hydrant flow test can be found in **Appendix E**.

8.3. Proposed Watermain Connection

The proposed development will be serviced by a 150 mm diameter fire and a 100 mm diameter domestic water service. According to City's standard drawing T-1104.02-3, the 150 mm water service will be split two (2) meters from the property line and valve and boxes will be installed on each service at the property line. The proposed water service will be connected to the existing 300 mm diameter watermain on the east side of Pharmacy Avenue. Refer to 'Proposed Servicing Plan' Figure-3 in Appendix F, for the proposed water connection.

9.0 Site Grading

9.1. Existing Grades

The site is currently occupied by of two (2) single-storey commercial buildings with outdoor parking area. Stormwater from the existing building's rooftop and parking area is captured by roof drains and by existing catchbasins respectively and is discharged into the City's infrastructure, on Pharmacy Avenue.

9.2. Proposed Grades

The proposed grades will improve the existing drainage conditions to meet the City's/Regional requirements. Grades will be maintained along the property line wherever feasible and emergency overland flow will be directed to Sheppard Avenue East. The owner shall be responsible to provide flood protection or a safe overland flow route for the proposed development without causing damage to the proposed and adjacent public and private properties. Existing drainage patterns on adjacent properties shall not be altered and stormwater runoff from the subject development shall not be directed to drain onto adjacent properties.

10.0 Conclusions and Recommendations

Based on our investigations, we conclude the following:

Storm Drainage

More details for the Stormwater Management (SWM) Section of this report will be prepared during the Site Plan Application stage. The site stormwater discharge will be controlled to the 2-year predevelopment flow and will be connected to the existing 675 mm diameter storm sewer on Pharmacy Avenue. In order to achieve the target flows and meet the City's Wet Weather Flow Management Guidelines (WWFMG), quantity controls will be utilized and up to 198.7 m³ of storage will be required. The stormwater management (SWM) system will be designed to provide enhanced level (Level 1) protection as specified by the Ministry of the Environment, Conservation and Parks (MECP). During Site Plan Application, a detailed analysis will be provided to assess the water quality on site and determine additional measures in order to achieve a minimum total suspended solids (TSS) removal of 80%.

Sanitary Sewers

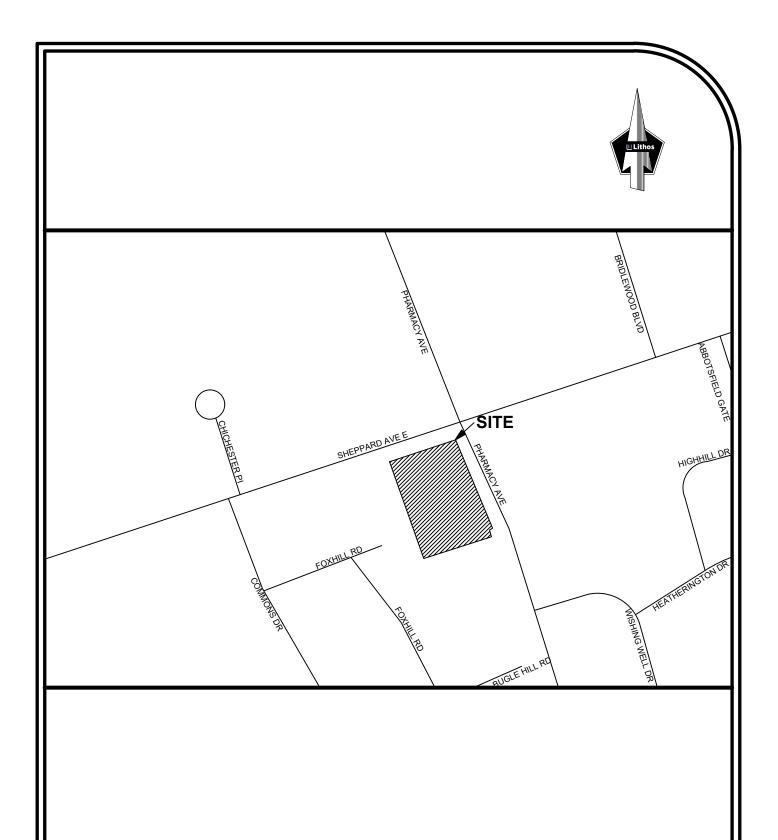
The flow from the proposed development will be directed to the existing 250 mm diameter sanitary sewer on Pharmacy Avenue. The additional net discharge flow from the proposed development, is anticipated at approximately 8.39 L/s. A Model Analysis is underway to determine the capacity of the existing sanitary sewer network along Pharmacy Avenue to accommodate the additional flow from the proposed development.

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Water Supply

Water supply for the site will be from the existing 300 mm diameter watermain on the east side of Pharmacy Avenue. It is anticipated that a total design flow of 136.26 L/s will be required to support the proposed development. The results of the hydrant flow test reveal that the existing water infrastructure can support the proposed development.





150 Bermondsey Road, North York, Ontario M4A 1Y1

LOCATION PLAN

MIXED USE DEVELOPMENT 2993-3011 SHEPPARD AVENUE EAST & 1800-1814 PHARMACY AVENUE TORONTO, ONTARIO

DATE:	SEPTEMBER 2019	PROJECT No:	UD18-057
SCALE:	N.T.S.	FIGURE No:	FIG 1







150 Bermondsey Road, North York, Ontario M4A 1Y1

AERIAL PLAN

MIXED USE DEVELOPMENT 2993-3011 SHEPPARD AVENUE EAST & 1800-1814 PHARMACY AVENUE TORONTO, ONTARIO

DATE:	SEPTEMBER 2019	PROJECT No:	UD18-057
SCALE:	N.T.S.	FIGURE No:	FIG 2

APPENDIX A Site Photographs



North-East Corner of the property along Pharmacy Avenue – Facing South-West

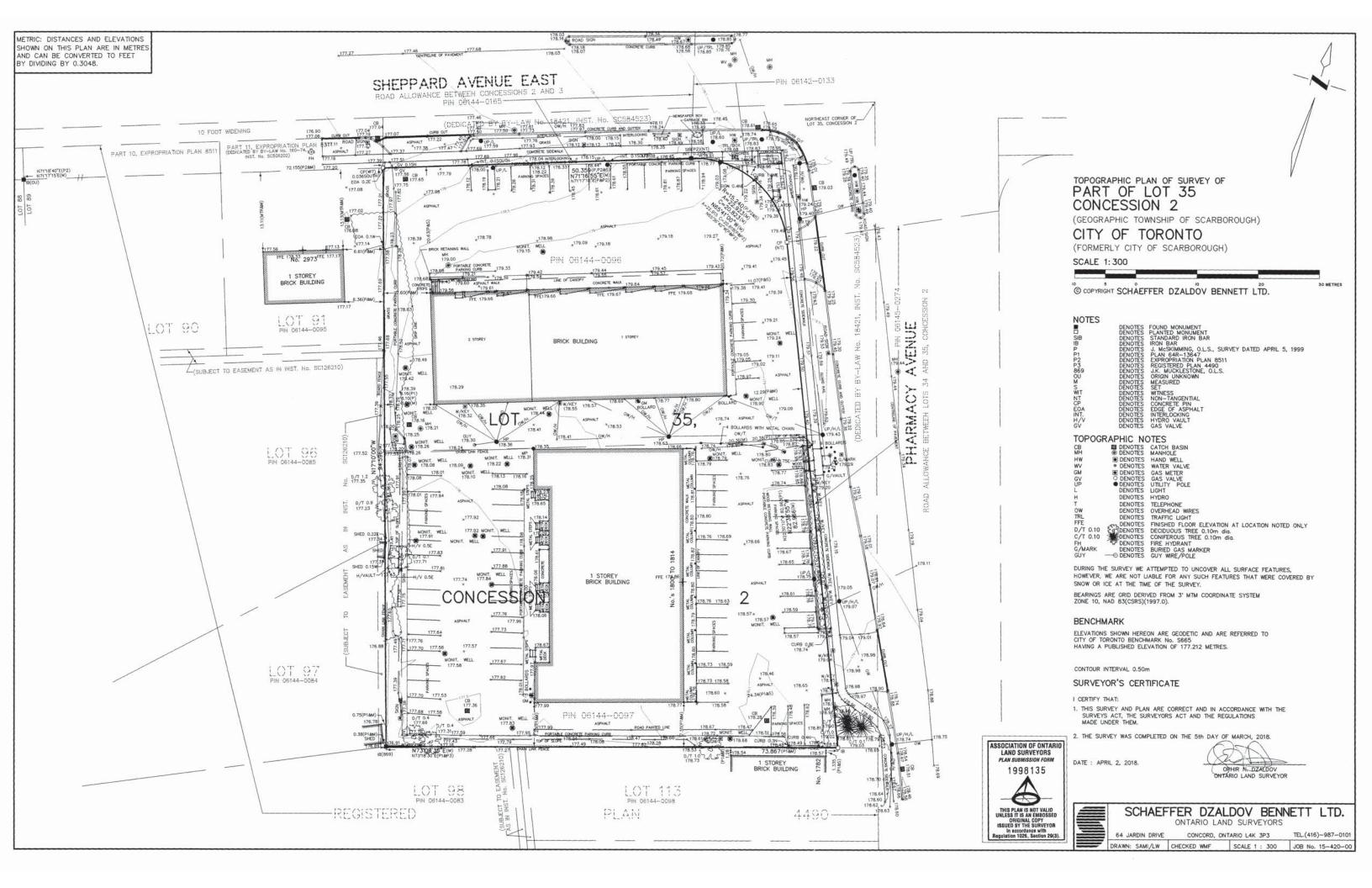


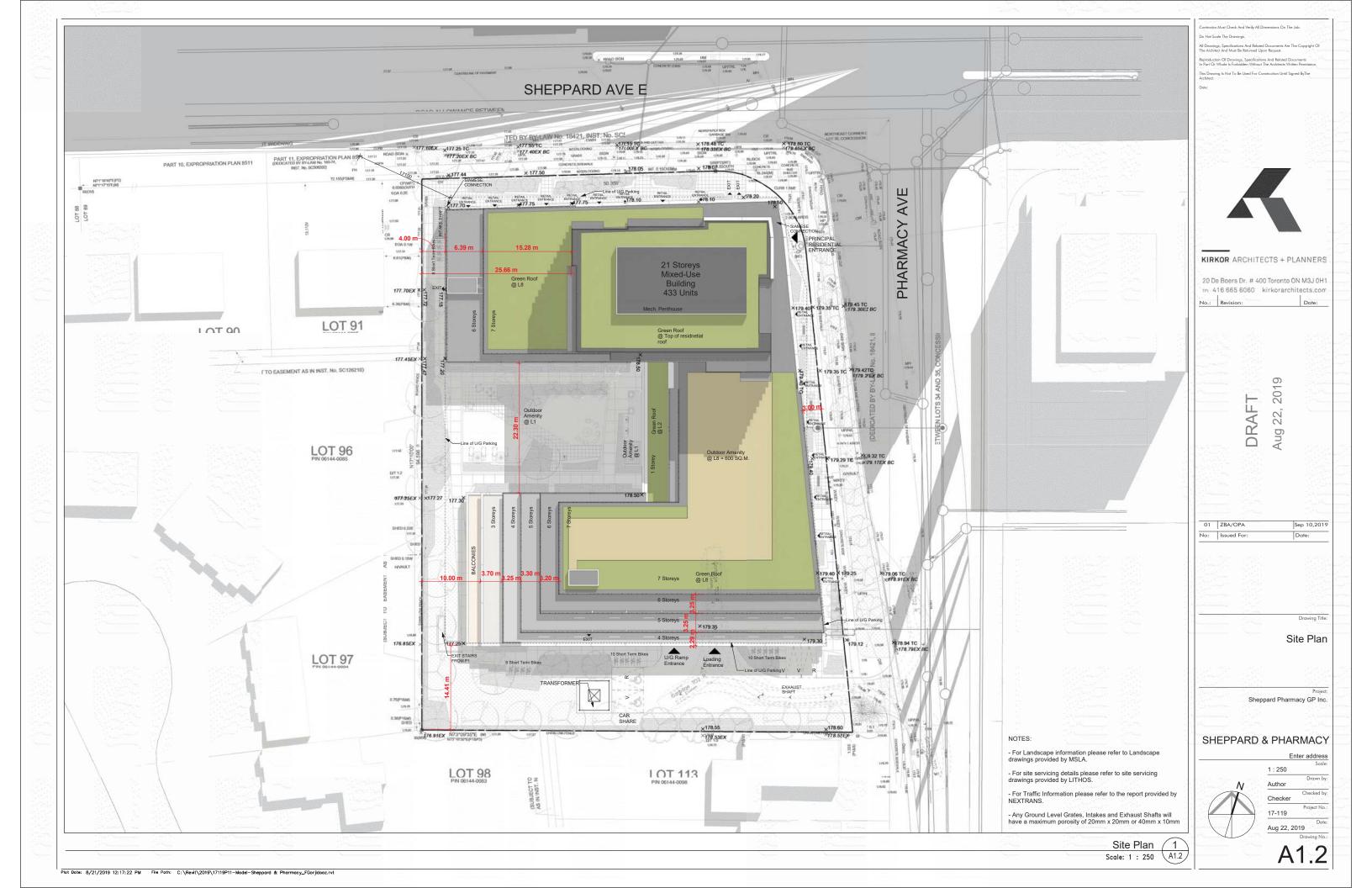
South-East Corner of the property along Pharmacy Avenue-Facing North-West



 $North-West\ Corner\ of\ the\ property\ along\ Sheppard\ Avenue\ East-Facing\ South-East$

APPENDIX B Background Information





Statistics Template - Toronto Green Standard Version 3.0 Mid to High Rise Residential and all New Non-Residential Development

The Toronto Green Standard Version 3.0 Statistics Template is submitted with Site Plan Control Applications and stand alone Zoning Bylaw Amendment applications. Complete the table and copy it directly onto the Site Plan submitted as part of the application.

For Zoning Bylaw Amendment applications: complete General Project Description and Section 1 d Section 2.

For Site Pl	an Control	applications	complete	General Proje	ct Description	, Section 1 and	d S
For further	informati	on, please vis	it www.tor	onto.ca/green	development		

General Project Description	Proposed
Total Gross Floor Area	29,308 m²
Breakdown of project components (m²)	
Residential	27,968 m²
Retail	1,340 m²
Commercial	
Industrial	
Institutional/Other	
Total number of residential units	433

Section 1: For Stand Alone Zoning Bylaw Amendment Applications and Site Plan Control Applications

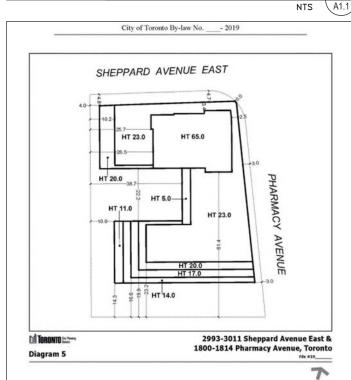
Automobile Infrastructure	Required	Proposed	Proposed %
Number of Parking Spaces	384	339	88.28
Number of parking spaces dedicated for priority LEV parking	1	1	100
Number of parking spaces with EVSE	68	68	100

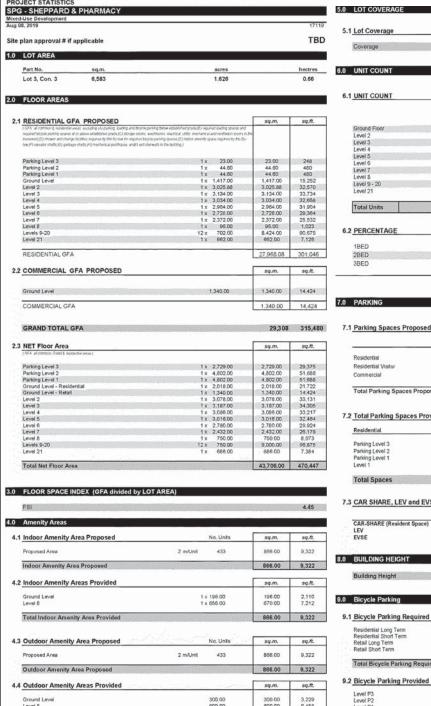
Cycling Infrastructure	Required	Proposed	Proposed %	
Number of long-term bicycle parking spaces (residential)	294	294	100	
Number of long-term bicycle parking spaces (all other uses)	2	2	100	
Number of long-term bicycle parking (all uses) located on:				
a) first storey of building		121		
b) second storey of building				
c) first level below-ground		75		
d) second level below-ground		75		
e) other levels below-ground		26		

Cycling Infrastructure	Required	Proposed	Proposed %
Number of short-term bicycle parking spaces (residential)	30	30	100
Number of short-term bicycle parking spaces (all other uses)	6	6	100
Number of male shower and change facilities (non-residential)			
Number of female shower and change facilities (non-residential)			
Tree Planting & Soil Volume	Required	Proposed	Proposed %



Toronto Green Standard Statistics 6



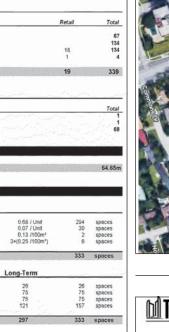


300.00 600.00 3,229 6,458 Total Bicycle Parking Provided

.0 LOT COVERAGE						
						,
5.1 Lot Coverage					sq.m.	sq.ft.
Coverage			57,8%		3,806.00	40,967
i.0 UNIT COUNT						
6.1 UNIT COUNT	192					
	F	18	28	38	Units/Floor	Total
Ground Floor		12	7	0	19	19
Level 2		22	22	2	46	46
Level 3 Level 4		23 23	22 21	2	47 46	47
Level 4 Level 5		23	19	2 2	46 45	46 45
Level 6		25	15	2	42	42
Level 7	Manager Manager	16	14	4	34	34
Level 8		0	0	0	0	0
Level 9 - 20		8	3	1	12	144
Level 21		4	4	2	10	10
Total Units						433
6.2 PERCENTAGE					Units in bldg.	Percen

1BED					245	56.6%
2BED					160	37.0%
3BED					28	6.5%
				-	433	100%
7.1 Parking Spaces Proposed Residential Residential Visitor	Ratio 0.60 A 0.14 J			No. of U 433 433	260 59	To spaces
7.1 Parking Spaces Proposed Residential	0.60 /		7.1	433	260 59	To spaces spaces spaces
Parking Spaces Proposed Residential Residential Visitor Commercial Total Parking Spaces Proposed	0.60 A 0.14 J			433 433	260 59 m 19	To spaces spaces spaces
7.1 Parking Spaces Proposed Residential Residential Visitor Commercial Total Parking Spaces Proposed 7.2 Total Parking Spaces Provided	0.60 A 0.14 J		Visitor	433 433	260 59 19 338	spaces spaces spaces
7.1 Parking Spaces Proposed Residential Residential Visitor Commercial Total Parking Spaces Proposed 7.2 Total Parking Spaces Provided Residential	0.60 A 0.14 J 1 Resident		Visitor	433 433	260 59 m 19	To spaces spaces spaces
7.1 Parking Spaces Proposed Residential Residential Visitor Commercial Total Parking Spaces Proposed 7.2 Total Parking Spaces Provided Residential Parking Level 3	0.60 A 0.14 A A Resident		Visitor	433 433	260 59 19 338	spaces spaces spaces
7.1 Parking Spaces Proposed Residential Residential Visitor Commercial Total Parking Spaces Proposed 7.2 Total Parking Spaces Provided Residential Parking Level 3 Parking Level 3 Parking Level 2	0.60 A 0.14 A 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		0.000	433 433	260 59 19 338 Retail	To spaces spaces spaces
7.1 Parking Spaces Proposed Residential Residential Visitor Commercial Total Parking Spaces Proposed 7.2 Total Parking Spaces Provided Residential Parking Level 3	0.60 A 0.14 A A Resident		Visitor	433 433	260 59 19 338	spaces spaces
Residential Residential Visitor Commercial Total Parking Spaces Proposed 7.2 Total Parking Spaces Provided Residential Parking Level 3 Parking Level 2 Parking Level 2 Parking Level 2	0.60 A 0.14 A A Resident 67 134 54		62	433 433	260 59 m 19 338 Retail	To spaces spaces spaces

Short-Term



Project Statistics 4 NTS A1.1

PART OF LOT 35, CONCESSION 2, (GEOGRAPHIC TOWNSHIP OF SCARBOROUGH), CITY OF TORONTO (FORMERLY CITY OF SCARBOROUGH)

> Legal Description 5 NTS



Context Plan 1 NTS

20 De Boers Dr. # 400 Toronto ON M3J 0H1 TFI 416 665 6060 kirkorarchitects.com

Context Plan (A1.1) NTS

M TORONTO . **Green Roof Statistics**

The Green Roof Statistics Template is required to be submitted for Site Plan Control Applications where a green roof is required under the Toronto Municipal Code Chapter 492. Green Roofs. Corrigide the table below and copy it directly onto the Roof Plan submitted as part of any Site Plan Control Application requiring a green roof in accordance with the Sylaw Refer to Section, 9492-1 of the Municipal Code for a corrigide list of defined terms, and greater clarify and certainty regarding the intent and application of the terms included in the template. The Toronto Municipal Code Chapter 492, Green Roofs can be found ordine at: https://doi.org/10.1008/nn.code/1184-492.pdf

Green Roof Statistics

		Proposed
Gross Floor Area, as defined in Green Roof Bylaw (m2)		29,308
Total Roof Area (m²)		3730.28
Area of Residential Private Terraces (m²)		865.20
Rooftop Outdoor Amenity Space, if in a Residential Building (m2)		600.00
Area of Renewable Energy Devices (m²)		
Tower (s)Roof Area with floor plate less than 750	m²	
Total Available Roof Space (m²)		226539
Green Roof Coverage	Required	Proposed
Coverage of Available Roof Space (m²)	1369.05	1360
Coverage of Available Roof Space (%)		60

Green Roof Statistics 3 NTS



KIRKOR ARCHITECTS + PLANNERS

Aug 22, 2019 DRAFI

Sep 10,2019 Date:

Context Plan, Site Statistics

Sheppard Pharmacy GP Inc.

SHEPPARD & PHARMACY

Author Checker

17-119 Aug 22, 2019

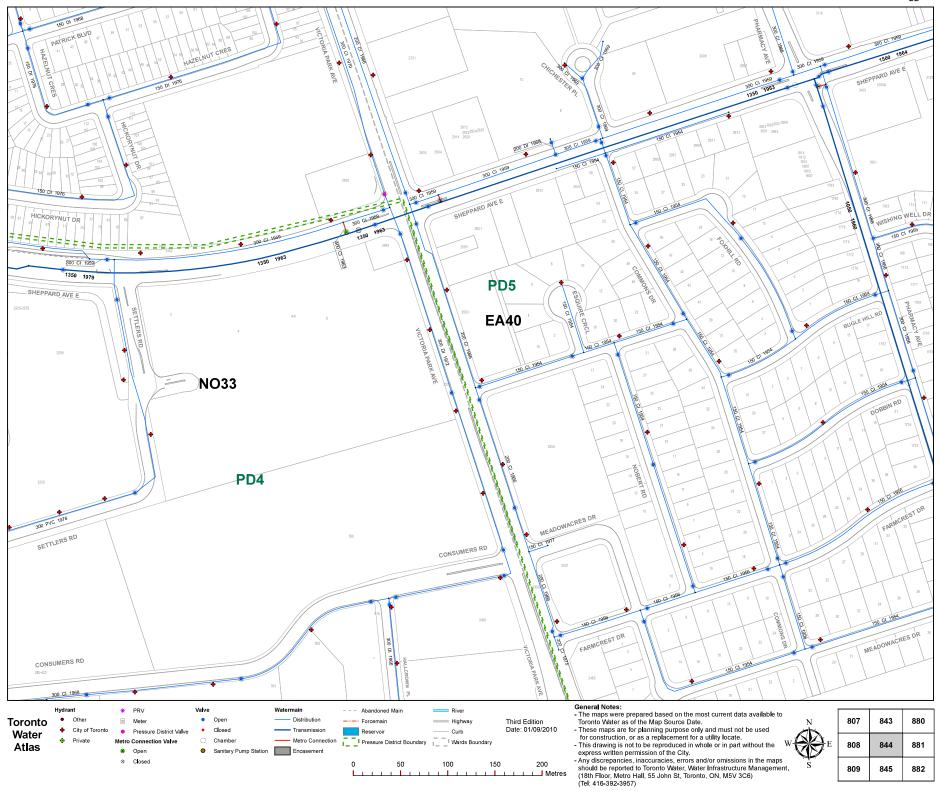
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Zoning Map prepared by BOUSFIELDS INC. 7

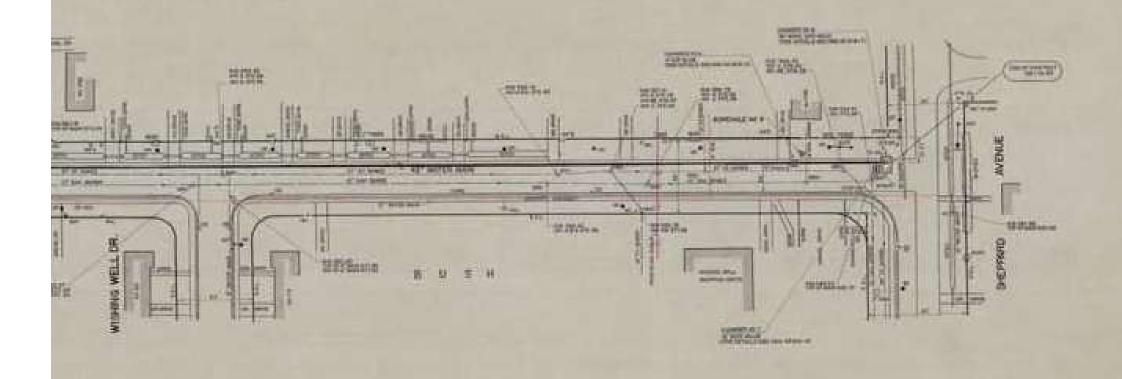
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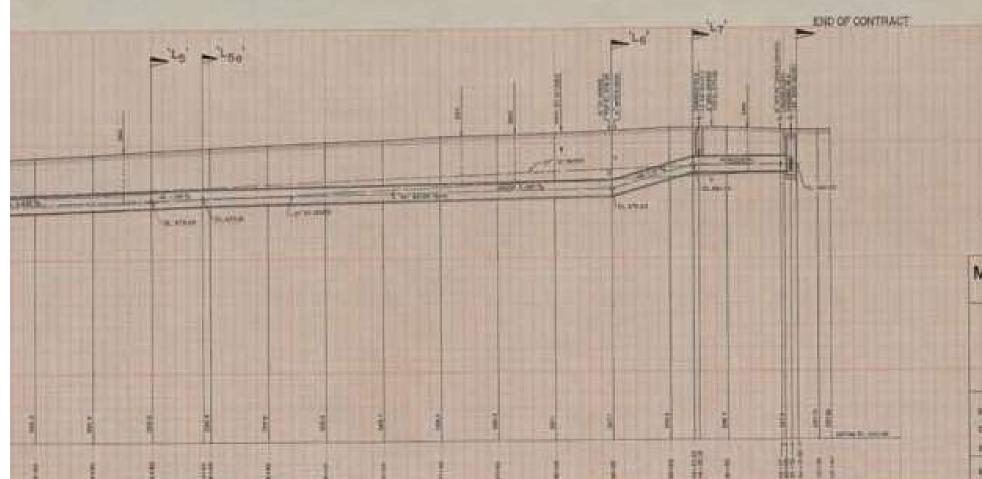






PART OF 61M-2





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NOTE ALL ELEVATIONS ARE GEODETIC

MUNICIPALITY OF METROPOLITAN TORONTO

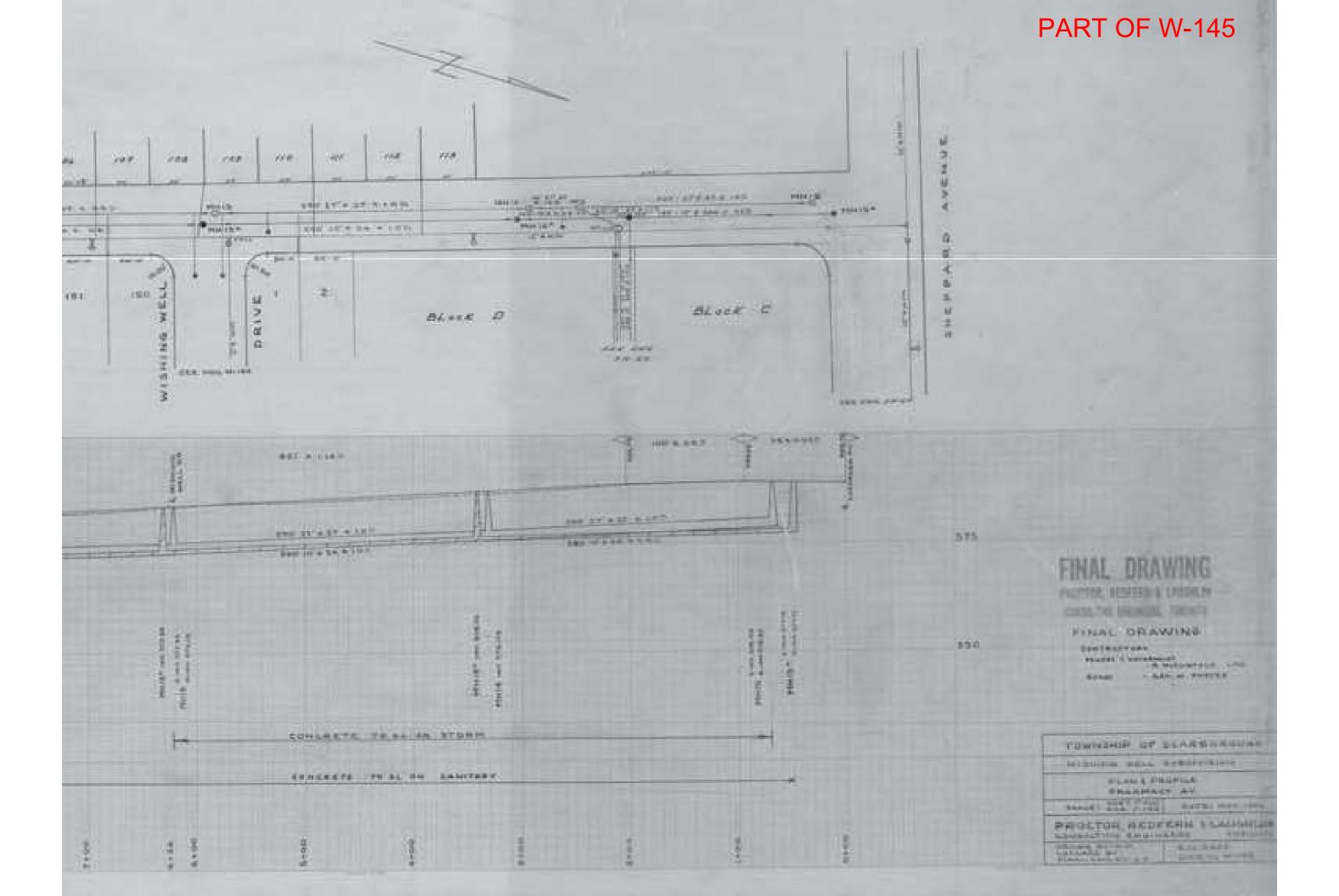
DEPARTMENT OF WORKS - WATER WORKS DIVISION

42 NOT WATER MAIN
ON PHARMACY AVENUE
FROM PACHINO BLVD. TO SHEPPARD AVE.

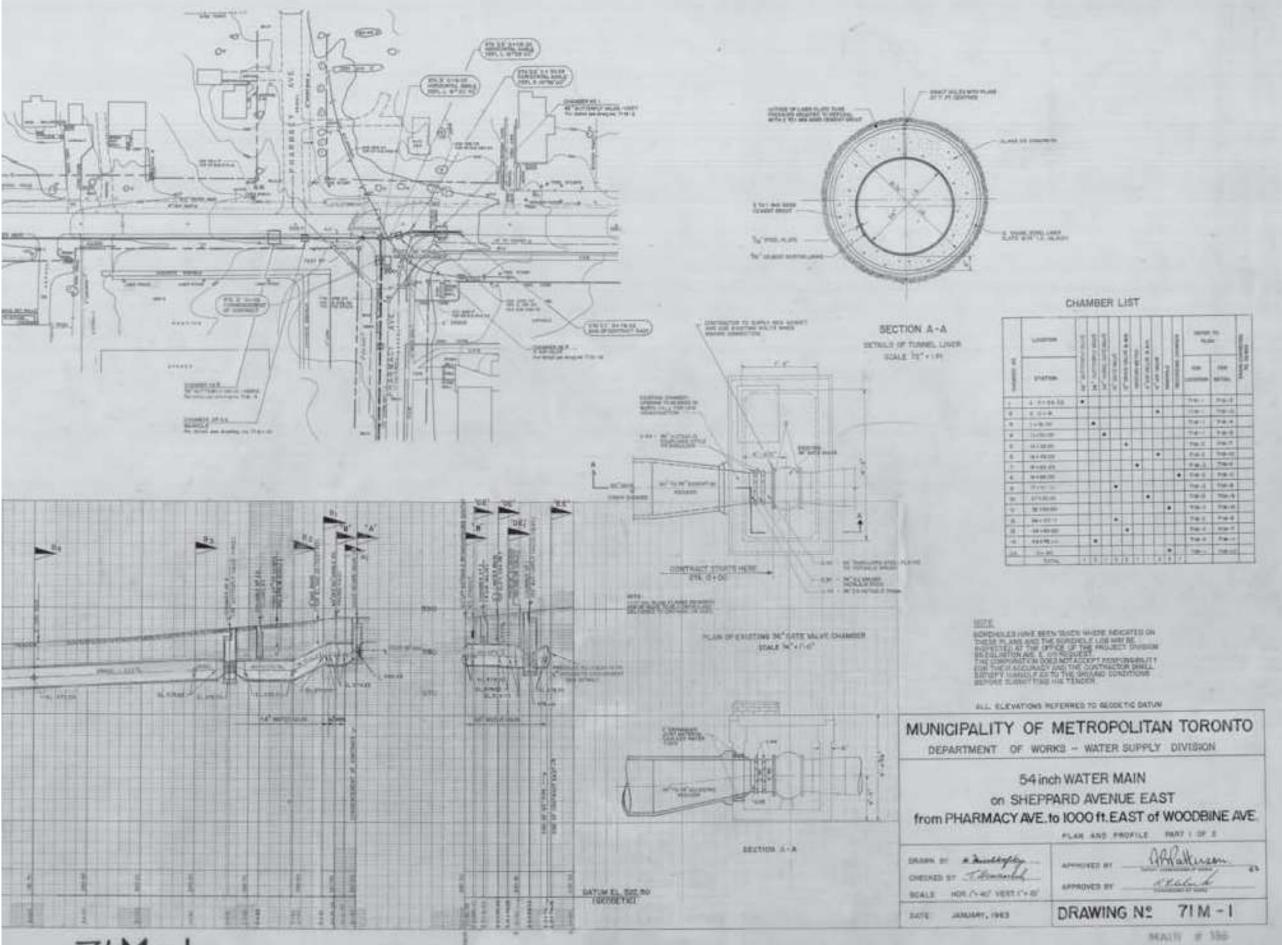
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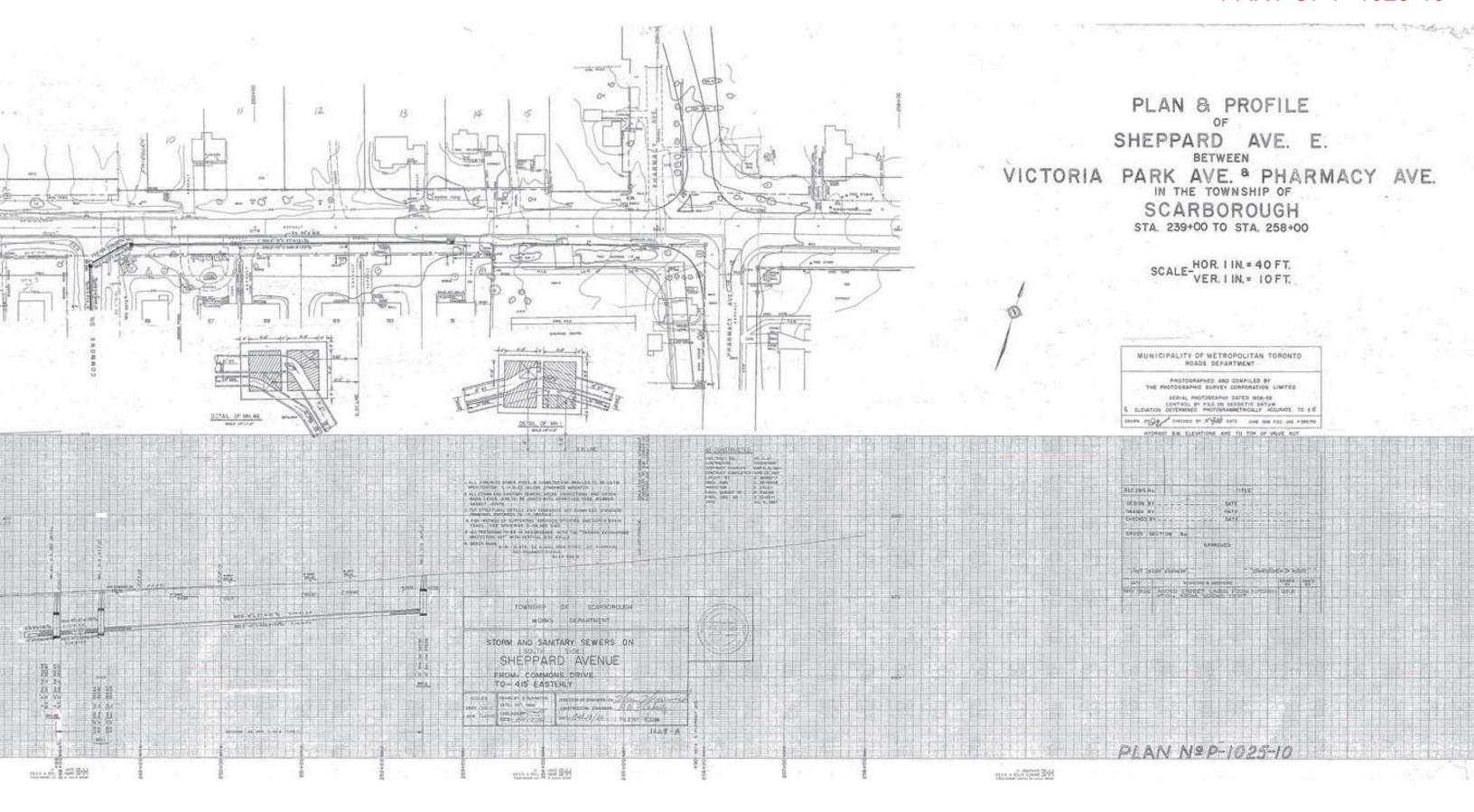
DRAWING Nº 61M-2

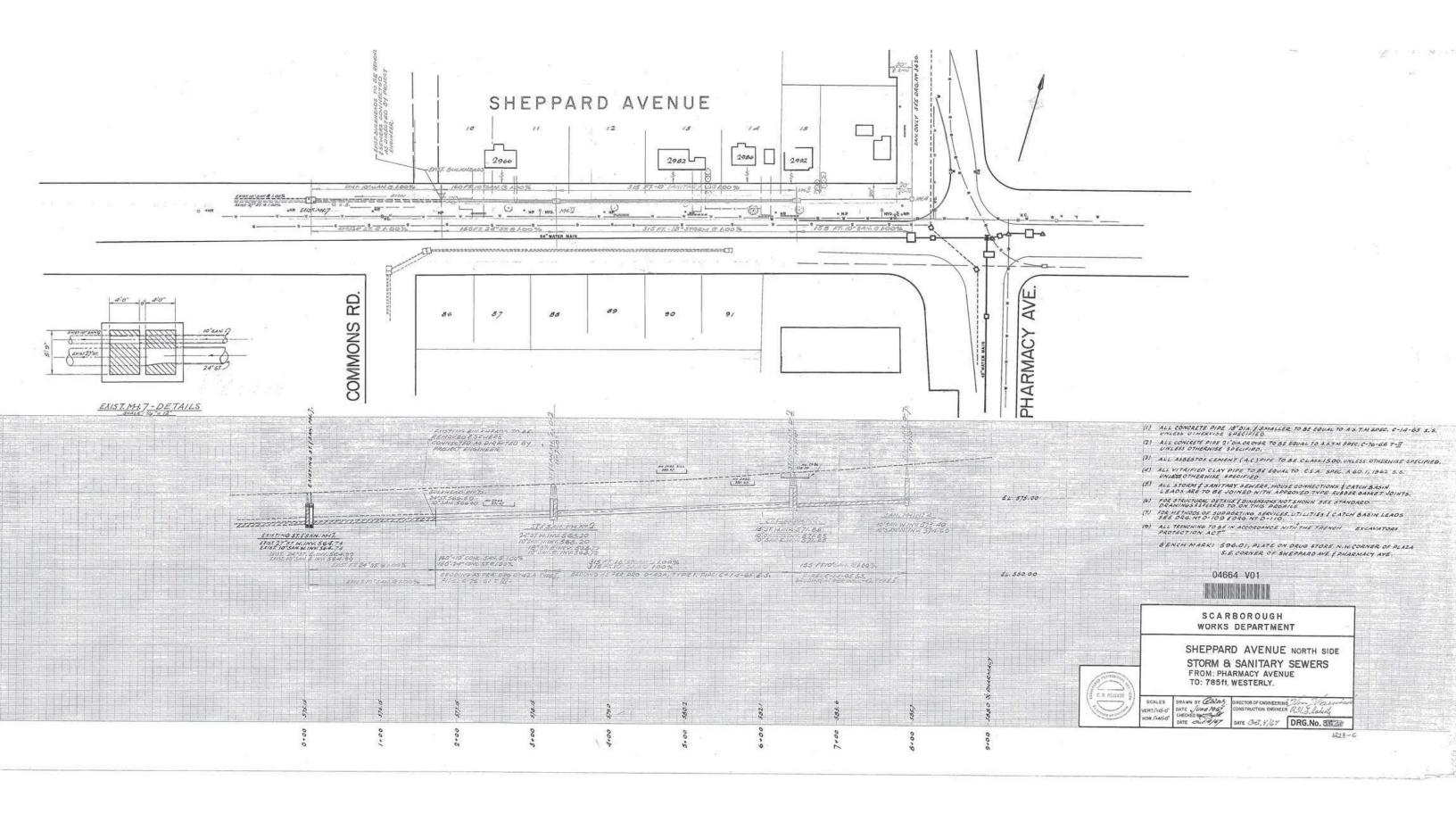


PART OF 71 M-1



PART OF P-1025-10





7.0 CONCLUSION AND RECOMMENDATIONS

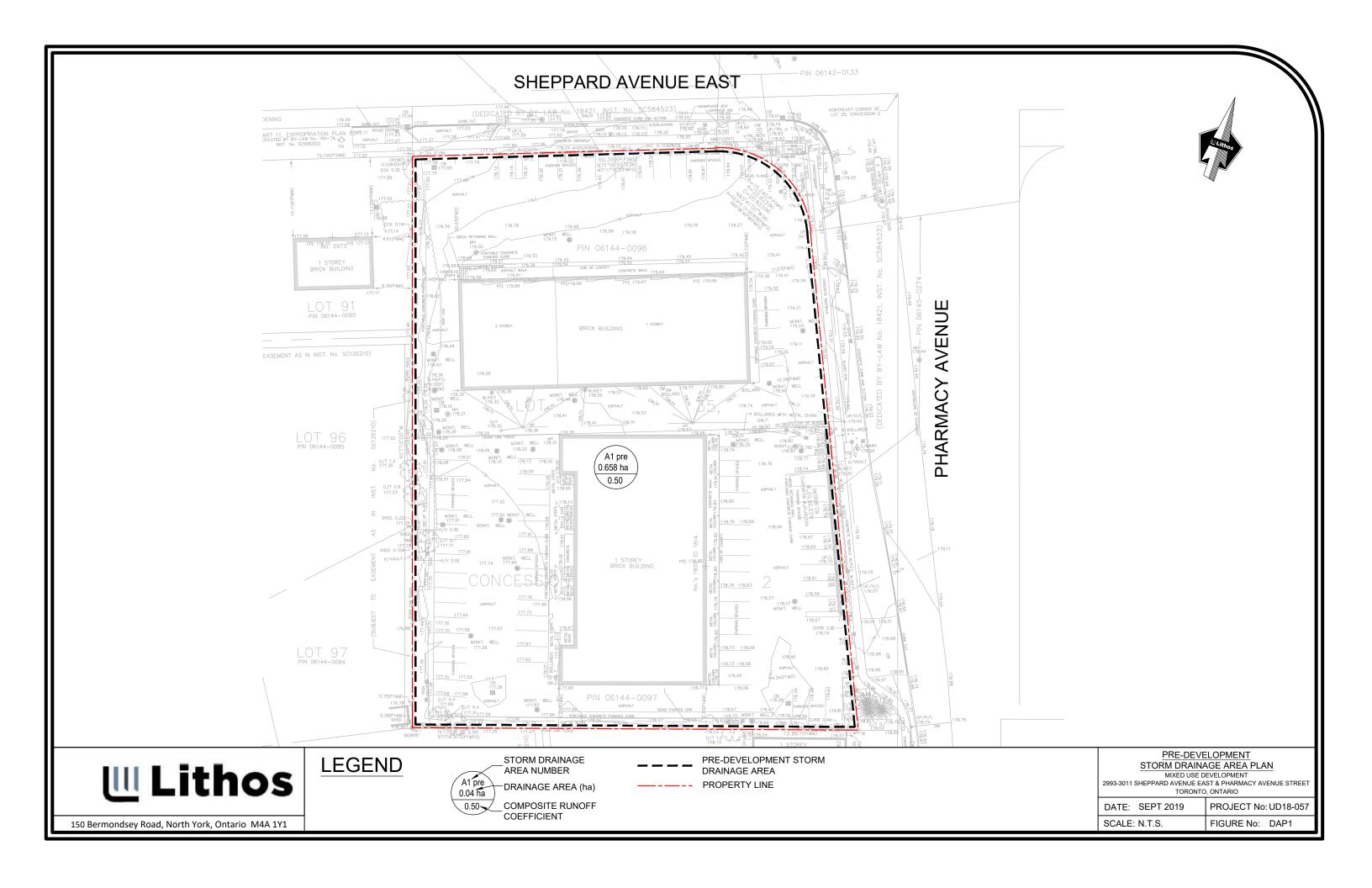
Based on the hydrogeological study completed, the following conclusions and recommendations are presented:

- The site is located in the Don River watershed. Regional ground water flow direction is towards the south towards Massey Creek located approximately 1 km south of the site. Based on the April 3, 3019 ground water monitoring results, shallow and intermediate horizontal ground water flow directions are towards the west.
- Ground water in on-site wells was measured at depths ranging from 0.67 to 13.02 m bgs (elevations ranging from 164.62 to 177.82 m amsl).
- According to MECP's WWIS database, no water supply well was present within 250 m of the proposed construction site. The site and surrounding areas are now serviced with municipal water and use of the water supply well, if any, is highly suspect. Hence, long-term impact to water wells in the area is not expected.
- The proposed site is not within any identified ground water quality threat areas based on the TRCA's approved source protection plan.
- No potential negative interference with the existing water takings is expected within 53 m radius from the site.
- The total dewatering rate during construction activities is estimated to be 101.3 m³/day, and is above the MECP threshold of 50 m³/day for an ESAR registration application but below the MECP threshold of 400 m³/day for a PTTW application. Therefore, an EASR is required during construction activities.
- The total dewatering rate during building occupancy is estimated to be 15.8 m³/day, and is below the MECP threshold of 50 m³/day for a PTTW application. Therefore, a PTTW is not required during building occupancy.
- The capacity of the municipal storm and sanitary sewer systems in the vicinity of the site is unknown; but, will be confirmed with the City of Toronto prior to the construction/dewatering/discharge activities.
- It is recommended that the dewatering system be designed by a qualified person and the dewatering operations be conducted by a licensed dewatering contractor.
- Discharge during dewatering operations can potentially be directed into the City of Toronto's sanitary and/or combined sewer system, or the storm sewer system after filtering, provided that a water discharge permit from the City of Toronto is obtained and that ongoing monitoring indicates that the discharge quality meets the relevant municipal sewer use by-law limits. Use of a GAC filtering system (at a minimum) may be necessary to remove VOC concentrations in ground water prior to discharging into municipal sewers.
- A ground water monitoring program should be implemented in the preconstruction, during construction and post construction phases. The monitoring program should include water

level measurement at frequent intervals and water quality monitoring of potentially vulnerable water supply wells, if any present nearby.

• A settlement monitoring program for adjacent structures located within the zone of influence (53 m) is suggested. Condition survey and monitoring program should be developed and carried out by a qualified consultant/surveyor.

APPENDIX C Storm Analysis





Rational Method Pre-Development Flow Calculation towards Addington Avenue

2993-3011 Sheppard Avenue East & 1800-1814 Pharmacy Avenue
City of Toronto
File No. UD18-057
Date: September 2019

Prepared By: Angelos Andreadis, P.E., M.A.Sc. Reviewed By: Nick Moutzouris, P.Eng., M.A.Sc.

Input Pa	arameters
----------	-----------

Area Number	Area (ha)	С	Tc (min.)		
A1 Pre	0.658	0.50	10		

Formula:		I = aT ^c						
	a,c	Constants						
	T	Time of concentration						
	I	Rainfall intensity						

Rational Method Calculation for the City of Toronto

Event 2-Year

a = 21.80 c = -0.78

Area Number	Α	С	AC	Tc	I	Q	Q
	(ha)			(min.)	(mm/h)	(m³/s)	(L/s)
A1 Pre	0.658	0.50	0.33	10	88.2	0.081	80.6

Event 5-Year

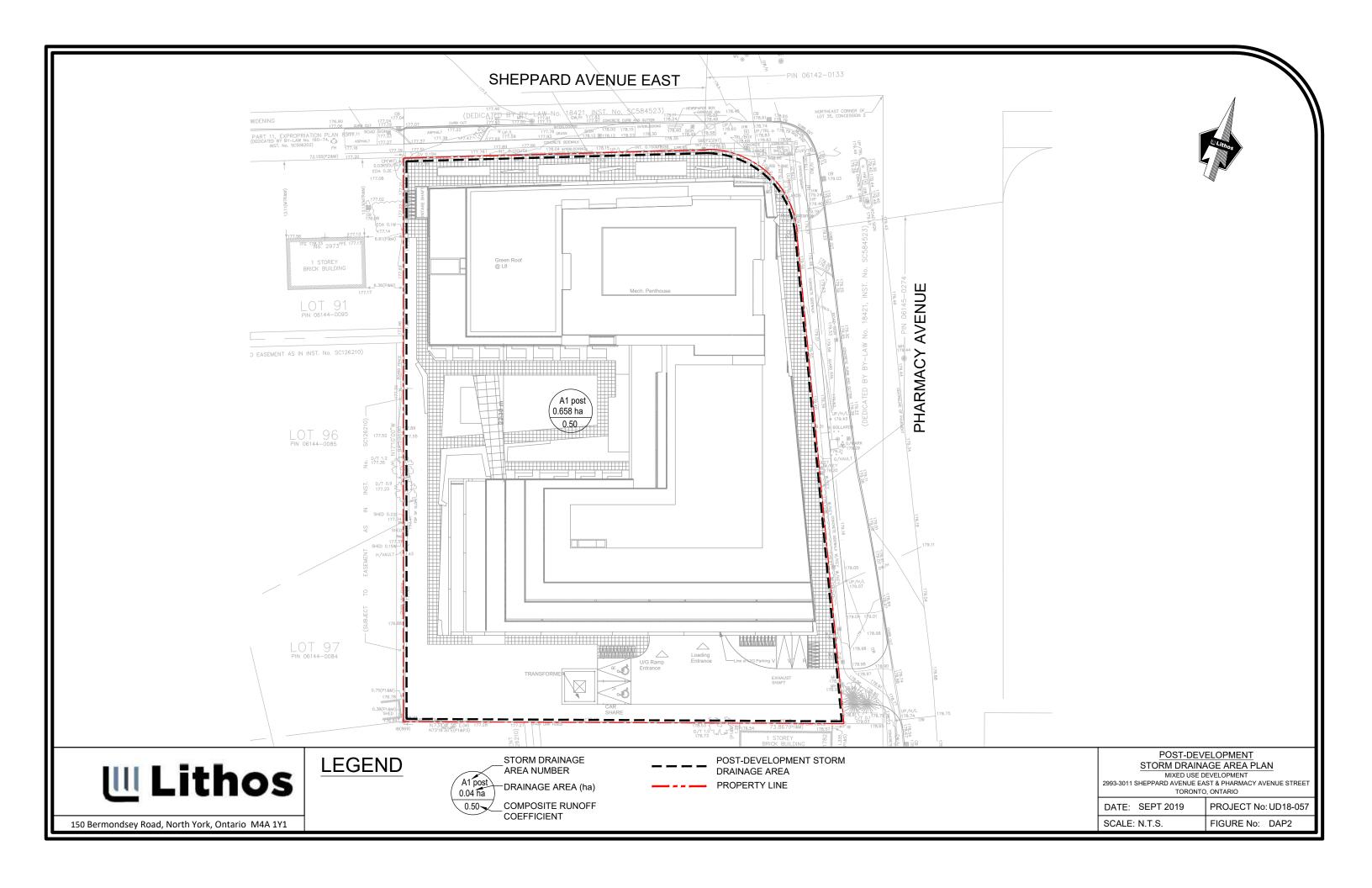
a = 32.00 c = -0.79

Area Number	Α	С	AC	Tc	I	I Q	
	(ha)			(min.)	(mm/h)	(m³/s)	(L/s)
A1 Pre	0.658	0.50	0.33	10	131.8	0.120	120.4

Event 100-Year

a = 59.70 c = -0.80

Area Number	A (ha)	С	AC	Tc (min.)	l (mm/h)	Q (m³/s)	Q (L/s)
A1 Pre	0.658	0.50	0.33	10	250.3	0.229	228.8





Modified Rational Method - Two Year Storm Site Flow and Storage Summary

2993-3011 Sheppard Avenue East & 1800-1814 Pharmacy Avenue File No. UD18-057 Date: September 2019

\sim	2440	ᅵᅵᄉฝ	A 4	Post
CO	nuo	nea	Αı	rosi

 Drainage Areas
 A1 Post

 Area (A1) =
 0.658
 ha

 "C" =
 0.90

AC1 = **0.592** Tc = **10.0**

Tc = **10.0** min
Time Increment = **5.0** min

Allowable Release Rate = 80.6 L/s Min.Storage = 38.7 m³

2 Year Design Storm

a= 21.80
c= -0.78
I= A(T)^c

(1)	(2)	(3)	(4)	(5)	(6)	
Time	Rainfall	Storm	Runoff	Runoff Target Released		
	Intensity	Runoff	Volume	Volume	Storage	
		(A1 Post)	(A1 Post)	(A1 Post)	(A1 Post)	
(min)	(mm/hr)	(m³/s)	(m ³)	(m ³)	(m³)	
10.0	88.2	0.145	87.04	48.36	38.69	
15.0	64.3	0.106	95.16	72.54	22.63	
20.0	51.4	0.084	101.38	96.71	4.67	
25.0	43.2	0.071	106.48	120.89	0.00	
30.0	37.4	0.062	110.84	145.07	0.00	
35.0	33.2	0.055	114.66	169.25	0.00	
40.0	29.9	0.049	118.08	193.43	0.00	
45.0	27.3	0.045	121.18	217.61	0.00	
50.0	25.1	0.041	124.02	241.78	0.00	
55.0	23.3	0.038	126.65	265.96	0.00	
60.0	21.8	0.036	129.10	290.14	0.00	
65.0	20.5	0.034	131.39	314.32	0.00	
70.0	19.3	0.032	133.55	338.50	0.00	
75.0	18.3	0.030	135.60	362.68	0.00	
80.0	17.4	0.029	137.53	386.86	0.00	
85.0	16.6	0.027	139.38	411.03	0.00	
90.0	15.9	0.026	141.14	435.21	0.00	
95.0	15.2	0.025	142.83	459.39	0.00	
100.0	14.6	0.024	144.45	483.57	0.00	
105.0	14.1	0.023	146.01	507.75	0.00	
110.0	13.6	0.022	147.52	531.93	0.00	
115.0	13.1	0.022	148.97	556.11	0.00	
120.0	12.7	0.021	150.37	580.28	0.00	
125.0	12.3	0.020	151.72	604.46	0.00	
130.0	11.9	0.020	153.04	628.64	0.00	
135.0	11.6	0.019	154.31	652.82	0.00	
140.0	11.3	0.019	155.55	677.00	0.00	
145.0	11.0	0.018	156.76	701.18	0.00	
150.0	10.7	0.018	157.93	725.35	0.00	
155.0	10.4	0.017	159.08	749.53	0.00	
160.0	10.1	0.017	160.19	773.71	0.00	
165.0	9.9	0.016	161.28	797.89	0.00	



Modified Rational Method - Five Year Storm Site Flow and Storage Summary

2993-3011 Sheppard Avenue East & 1800-1814 Pharmacy Avenue File No. UD18-057 Date: September 2019

Controlled A1 Post

 Drainage Areas
 A1 Post

 Area (A1) =
 0.658
 ha

 "C" =
 0.90

 AC1 =
 0.592

Tc = 10.0 min
Time Increment = 5.0 min

81.7

 m^3

Allowable Release Rate = **80.6** L/s

Min.Storage =

5 Year Design Storm

a= 32.00
c= -0.79
I= A(T)°

(1)	(2)	(3)	(4)	(5)	(6)
Time	Rainfall	Storm	Runoff	Target Released	Total Required
	Intensity	Runoff	Volume	Volume	Storage
		(A1 Post)	(A1 Post)	(A1 Post)	(A1 Post)
(min)	(mm/hr)	(m³/s)	(m³)	(m ³)	(m ³)
10.0	131.8	0.217	130.08	48.36	81.72
15.0	95.7	0.157	141.64	72.54	69.10
20.0	76.2	0.125	150.46	96.71	53.75
25.0	63.9	0.105	157.68	120.89	36.79
30.0	55.3	0.091	163.83	145.07	18.76
35.0	49.0	0.081	169.22	169.25	0.00
40.0	44.1	0.073	174.04	193.43	0.00
45.0	40.2	0.066	178.39	217.61	0.00
50.0	37.0	0.061	182.39	241.78	0.00
55.0	34.3	0.056	186.07	265.96	0.00
60.0	32.0	0.053	189.50	290.14	0.00
65.0	30.0	0.049	192.72	314.32	0.00
70.0	28.3	0.047	195.74	338.50	0.00
75.0	26.8	0.044	198.60	362.68	0.00
80.0	25.5	0.042	201.31	386.86	0.00
85.0	24.3	0.040	203.88	411.03	0.00
90.0	23.2	0.038	206.35	435.21	0.00
95.0	22.3	0.037	208.70	459.39	0.00
100.0	21.4	0.035	210.96	483.57	0.00
105.0	20.6	0.034	213.14	507.75	0.00
110.0	19.8	0.033	215.23	531.93	0.00
115.0	19.1	0.031	217.25	556.11	0.00
120.0	18.5	0.030	219.20	580.28	0.00
125.0	17.9	0.029	221.08	604.46	0.00
130.0	17.4	0.029	222.91	628.64	0.00
135.0	16.9	0.028	224.69	652.82	0.00
140.0	16.4	0.027	226.41	677.00	0.00
145.0	15.9	0.026	228.08	701.18	0.00
150.0	15.5	0.026	229.71	725.35	0.00
155.0	15.1	0.025	231.30	749.53	0.00
160.0	14.7	0.024	232.85	773.71	0.00
165.0	14.4	0.024	234.36	797.89	0.00



Modified Rational Method - Hundred Year Storm Site Flow and Storage Summary

2993-3011 Sheppard Avenue East & 1800-1814 Pharmacy Avenue File No. UD18-057 Date: September 2019

Controlled A1 Post

Drainage Areas A1 Post
Area (A1) = 0.658 ha
"C" = 0.90
AC1 = 0.592

AC1 = **0.592** Tc = **10.0**

Tc = **10.0** min
Time Increment = **5.0** min

Allowable Release Rate = 80.6 L/s Min.Storage = 198.7 m³

 100 Year Design Storm

 a=
 59.70

 c=
 -0.80

 l=
 A(T)^c

(1)	(2)	(3)	(4)	(4) (5)			
Time	Rainfall	Storm	Runoff	Target Released	Total Required		
	Intensity	Runoff	Volume	Volume	Storage		
		(A1 Post)	(A1 Post)	(A1 Post)	(A1 Post)		
(min)	(mm/hr)	(m ³ /s)	(m ³)	(m ³)	(m ³)		
10.0	250.3	0.412	247.07	48.36	198.71		
15.0	181.0	0.298	267.94	72.54	195.40		
20.0	143.8	0.237	283.80	96.71	187.09		
25.0	120.3	0.198	296.76	120.89	175.86		
30.0	103.9	0.171	307.78	145.07	162.71		
35.0	91.9	0.151	317.41	169.25	148.16		
40.0	82.6	0.136	326.01	193.43	132.58		
45.0	75.1	0.124	333.78	217.61	116.17		
50.0	69.1	0.114	340.88	241.78	99.10		
55.0	64.0	0.105	347.44	265.96	81.48		
60.0	59.7	0.098	353.54	290.14	63.40		
65.0	56.0	0.092	359.25	314.32	44.93		
70.0	52.8	0.087	364.61	338.50	26.11		
75.0	49.9	0.082	369.68	362.68	7.00		
80.0	47.4	0.078	374.48	386.86	0.00		
85.0	45.2	0.074	379.05	411.03	0.00		
90.0	43.2	0.071	383.41	435.21	0.00		
95.0	41.3	0.068	387.58	459.39	0.00		
100.0	39.7	0.065	391.57	483.57	0.00		
105.0	38.2	0.063	395.41	507.75	0.00		
110.0	36.8	0.060	399.11	531.93	0.00		
115.0	35.5	0.058	402.67	556.11	0.00		
120.0	34.3	0.056	406.11	580.28	0.00		
125.0	33.2	0.055	409.44	604.46	0.00		
130.0	32.2	0.053	412.67	628.64	0.00		
135.0	31.2	0.051	415.79	652.82	0.00		
140.0	30.3	0.050	418.83	677.00	0.00		
145.0	29.5	0.048	421.78	701.18	0.00		
150.0	28.7	0.047	424.65	725.35	0.00		
155.0	27.9	0.046	427.44	749.53	0.00		
160.0	27.2	0.045	430.17	773.71	0.00		
165.0	26.6	0.044	432.82	797.89	0.00		

APPENDIX D Sanitary Data Analysis



SANITARY SEWER DESIGN SHEET

2993-3011 Sheppard Avenue East & 1800-1814 Pharmacy Avenue

CITY OF TORONTO

				RE	SIDENTIA	ΔI				COMM	ERCIAL	Ī			FLO ¹	W				Ī		EWED	DESIGN	
	SECTION	1			MBER OF UN				SECTION	COMM.	SECTION	TOTAL	AVERAGE	HARMON	RES. PEAK	AVERAGE	TOTAL	INFILT.	TOTAL	PIPE	PIPE	PEVVER	FULL FLOW	0/ .f.DE010
LOCATION	AREA	Single Fam. Dwell.	Townhouse	Studio	GU units		2 Bed Apts.	3 Bed Apts.	POP.	AREA	POP. @ 110 ppha	ACCUM. POP.	RESIDENTIAL FLOW '@' 240 L/c/d	PEAKING FACTOR	FLOW	COMMERCIAL FLOW @ 250 L/c/d	ACCUM.	@ 0.26 L/s/ha.	DESIGN FLOW	LENGTH	DIA.	SLOPE	CAPACITY n = 0.013	% of DESIG CAPACITY
	(ha.)	@ 3.5 ppu	@ 2.7	@ 1.4 ppu	@ 3.1 ppu	@ 1.4 ppu	@ 2.1 ppu	@ 3.1 ppu	(persons)	(ha.)	(persons)	(persons)	(L/s)		(L/s)	(L/s)	(ha.)	(L/s)	(L/s)	(m)	(mm)	(%)	(L/sec)	(%)
column number	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
Existing Condition																								
Retail	0.658	0	0	0	0	0	0	0	0	0.241	27	27	0.00	4.50	0.00	0.077	0.658	0.171	0.25					
Proposed Condition																								
Mixed-Use	0.658	0	0	0	0	245	160	28	766	0.134	15	781	2.13	3.87	8.24	0.043	0.658	0.171	8.45		200	2.0%	46.38	19%
Groundwater																			0.18					
					_												Total Ne	et Flow	8.39					
Commercial Flow Rate - 2 Residential Flow Rate - 24																								
Infiltration - 0.26 L/ha	40 IIII ES/C	apita/uay																						
Peaking Factor = 1 + [14] Site Area:	/ (4 + P ^{0.5})] 0.658		ation in tho	ousands																				
		-	Prepared	d by: Ar	ngelos A	ndreadis	s, P.E., I	M.A.Sc.			1	Project:	2993-3011	Sheppar	d Avenu	e East & 180	0-1814	Pharm	nacy Ave	nue				<u>I</u>
IIII Litk	105		Reviewe	-	-							_	UD18-057	• •					•					



Date: September 2019

City of Toronto

Sheet 1 OF 1

APPENDIX E Water Data Analysis



WATER DEMAND

2993-3011 Sheppard Avenue East & 1800-1814 SPharmacy Avenue

File No: UD18-057 Date: September 2019

Prepared by: Angelos Andreadis, P.E., M.A.Sc. Reviewed By: Nick Moutzouris, P.Eng., M.A.Sc.

with the largest areas

Note 1: The levels indicated, reference the floors

Fire Flow Calculation

1 F= 220 C (A)^{1/2}

Where F= Fire flow in Lpm

C= construction type coefficient

= 0.6 fire resistive construction

A = total floor area in sq.m. including basement (main use)

Area Applied

Level 02= 3078.0 m² 100% Ground Floor= 3358.0 m² 25% Level 03= 3187.0 m² 25%

A = 4,714 sq.m.

F = 9,063.17 L/min F(No.1) = 200CVA

F = 9,000 L/min F(No.1) Round to nearest 1000 l/min

2 Occupancy Reduction

15% reduction for limited-combustible occupancy

F = 7650 L/min $F(No.2) = F(No.1) \times \text{occupancy reduction/charge(%)}$

3 Sprinkler Reduction

30% Reduction for NFPA Sprinkler System

F = 5355 l/min $F(No.3) = F(No.2) \times \text{sprinkler reduction}(\%)$

4 Separation Charge

 20% West
 3.1m to 10.0m

 0% North
 Road

 20% South
 3.1m to 10.0m

 0% East
 Road

 40% Total Separation Charge

F = 3,060.00 L/min $F (No.4) = F(No.2) \times \text{separation charge}(\%)$

F = 8,415.00 L/min F(tot) = F(No.3) + F(No.4)

F = 8,000 L/min F(tot) Round to nearest 1000 l/min

133.33 L/s F = 2114 US GPM

Domestic Flow Calculations

Population = 766 from Sanitary Design Sheet

Retail Area= 1340 from Site Statistics

Average Day Demand = 191 L/cap/day

= $5 \text{ L/m}^2/\text{day}$ (OBC)

1.77 L/s

28 US GPM 1 US GPM=15.852L/s

Max. Daily Demand Peaking Factor = 1.65

Max. Daily Demand = 2.92 L/s = 46 US GPM

or

Max. Hourly Demand Peaking Factor = 2.48

Max. Hourly Demand = 4.39 L/s = 70 US GPM

Max Daily Demand = 2.92 L/s Fire Flow = 133.33 L/s

Required 'Design' Flow = 136.26 L/s 2160 US GPM

Note: Required 'Design' Flow is the maximum of either:

1) Fire Flow + Maximum Daily Demand

1 US Gallon=3.785 L

2) Maximum Hourly Demand



WATER DEMAND

2993-3011 Sheppard Avenue East & 1800-1814 SPharmacy Avenue

File No: UD18-057

Date: September 2019

Prepared by: Angelos Andreadis, P.E., M.A.Sc. Reviewed By: Nick Moutzouris, P.Eng., M.A.Sc.

Pressure Losses

Hazen-Williams Formula

 $V = kCR_h^{0.63}xS^{0.54}$

k = 0.85- conversion factor (0.849 for SI units and 1.318 for US customary units)

C= 150 - roughness coefficient (PVC: 140-150)

S= h_f/L

- hydraulic radius (D/4 for full flow, A/P_W for partially flow) Rh= D/4

Fire Fighting and Domestic Head Loss

Flow Requirements= 136.26 L/s 150 mm Diameter= Area= 1.77E-02 L= 5 m 7.71 m/s V= S= 2.56E-01

> R_h= 0.04 1.28 m $H_f =$ 1.82 psi

Flow Test (dated: June 7, 2019)

when: Static Pressure = 56 psi Flow = 0 gpm = 73.37 Residual Pressure = 48 psi Flow = 1163 gpm =

Pressure

(psi) Flow (L/s) Based on the Pressure/Flow relationship, we have to confirm that the flow requirement of 136.26 L/s can be provided at minimum pressure (20.3 psi + Losses) as set out by the FUS 56 0.0 48

73.4 guidelines

22.12 psi (20.3+Hf) 30.8 136.26 Fire Flow is above minimum of

Since the flow of 136.26 L/s required for the proposed development is provided in the existing watermain at 30.8 psi (which is more than the minimum of 22.12 psi), the existing watermain infrastructure can support the proposed development.

> Flow available at 20psi = 2,620 gpm = 165.30 L/s

> > Q_{avail} @ 20psi = $Q_T ((P_S-P_A)/(P_S-P_R))^{0.54}$ = $1163 \times ((56-20)/(56-48))^{0.54}$ 2,620 gpm



HYDRANT FLOW TESTING

NOTE:Hydrants tested according to NFPA 291: Recommended Practice for Fire Flow Testing and Marking of Hydrants

GENERAL INFORMATION

General Information

Date of TestingJun 7, 2019Project Number:2019-0185

Site Location / Address: 3005 Sheppard

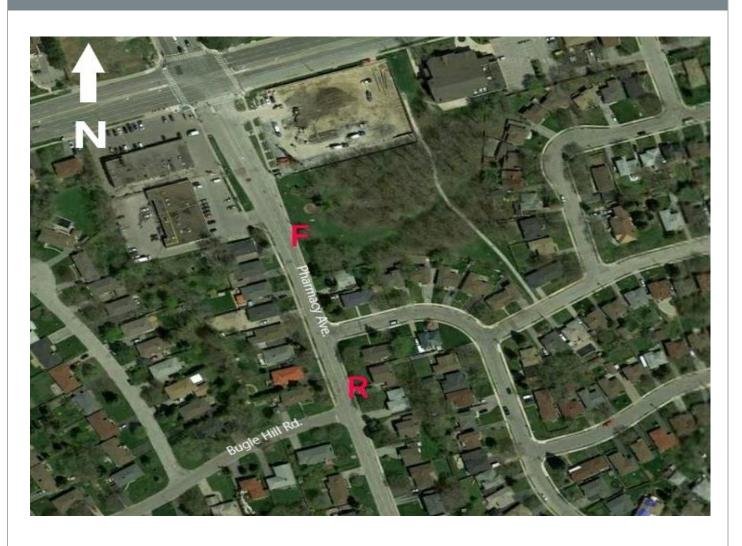
Region / Municipality Toronto

Hydrants Opened By: Toronto Water

Tested by:Matt B
Dave V

HYDRANT TEST INFORMATION

Hydrant Test Location - Residual Hydrant=R, Flow Hydrant=F



Test Data

Time of Test 8:32 AM

Pipe Size (mm) 300

Flow Hydrant Test Location (description)

Across street from 1782 Pharmacy Ave

Residual Hydrant Test Location (description) 1773 Pharmacy Ave

Q1 Test Data (1 Orifice)

Static Pressure(PSIG)

# OUTLETS	ORIFICE SIZE(IN)	PITOT PRESSURE(PSIG)	FLOW(USGPM)	RESIDUAL PRESSURE(PSIG)
1	2.5	30	919	50

QT Test Data (2 Orifices)

# OUTLETS	ORIFICE SIZE(IN)	PITOT PRESSURE(PSIG)	FLOW(USGPM)	RESIDUAL PRESSURE(PSIG)
2	2.5	12	1163	48

Calculations

Q= 29.83 cd^2√p

Where:

c- coefficient of discharge (1 in smooth pipe)

d- pipe diameter (inches)

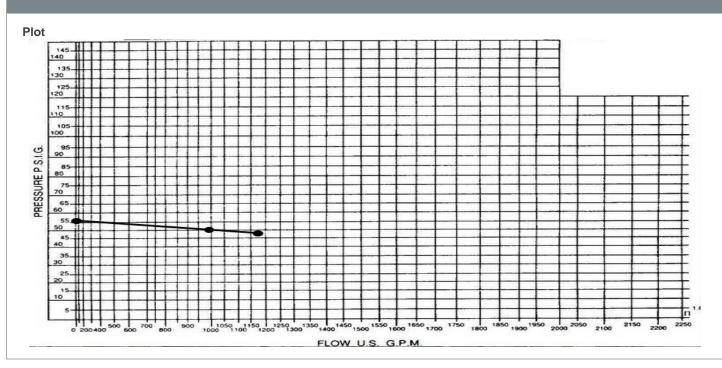
p- pitot reading (psig)

Q1 - 1 Orifice(s) Q1= $(29.83)(0.9)(2.5)^2 \sqrt{30}=919$

QT - 2 Orifice(s) Q1= $(29.83)(0.9)(2.5)^2 \sqrt{12}=1163$

Static Pressure(PSIG) 5

Test Results



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APPENDIX F Engineering Drawings

